Energy Modeling of Dedicated Outdoor Air Systems for a Small Commercial Pilot Project

BUILDING ENERGY SIMULATION FORUM, JUNE 19, 2019 AMY MONTGOMERY, MASc, P.Eng.



Overview

→ Pilot project: energy efficient replacement options for end-of-life packaged rooftop units on small commercial buildings



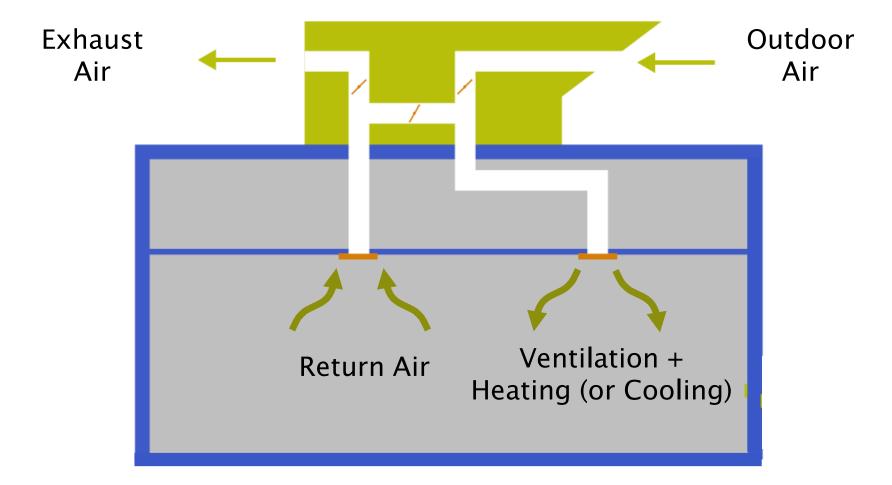
- → Dedicated Outdoor Air Systems (DOAS) with Heat Recovery Ventilation (HRV)
- → Energy modeling as a tool to quantify savings
- → Share progress and lessons learned

- → Target Building Sector:
 - → Small commercial (< 25,000 ft²)
 - → Includes small office, retail, schools, restaurants, small assembly
 - → Makes up approx. half of the commercial building floor area in the Pacific Northwest.
 - → Smaller HVAC systems; typically not engineered.



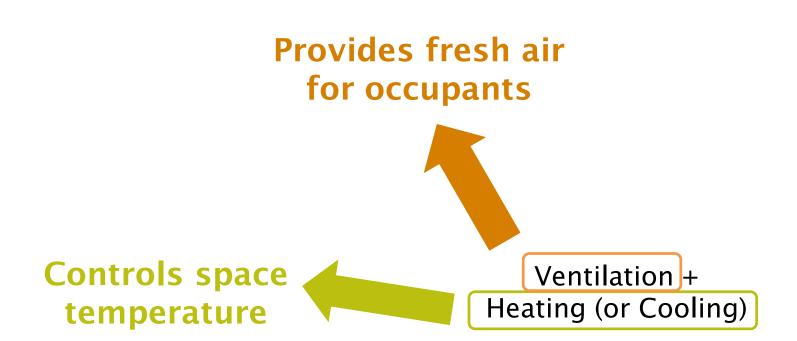
- → Dedicated Outdoor Air System (DOAS) with Heat Recovery in Small Commercial Building Sector
- → Early pilot work funded by the Northwest Energy Efficiency Alliance (NEEA)
 - → New high efficiency HRV (> 0.85 eff @ 75% max flow)

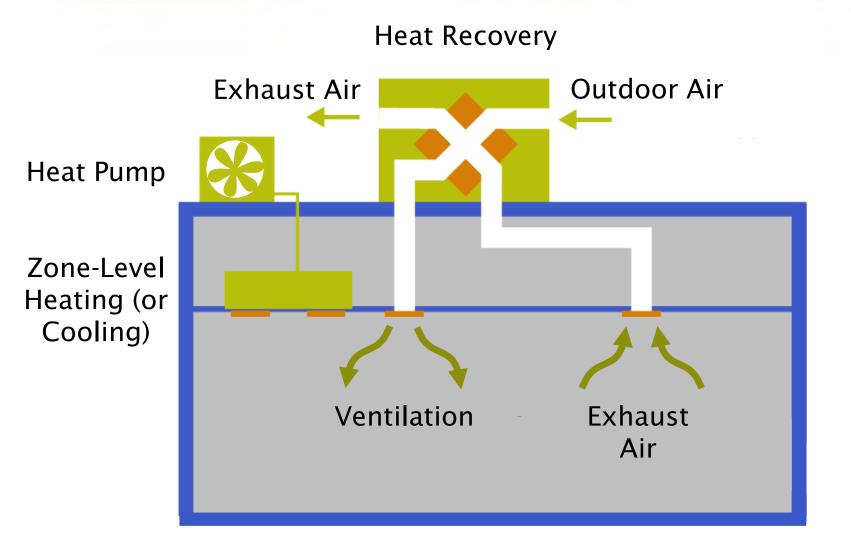




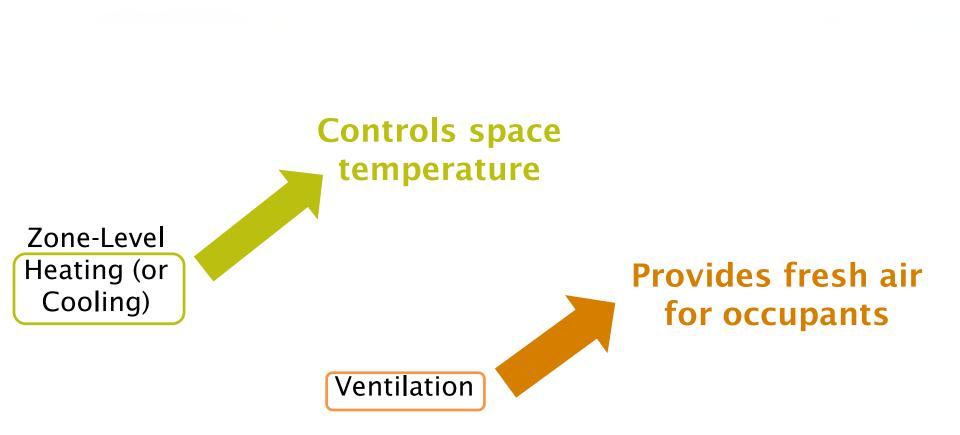
Packaged Rooftop Unit



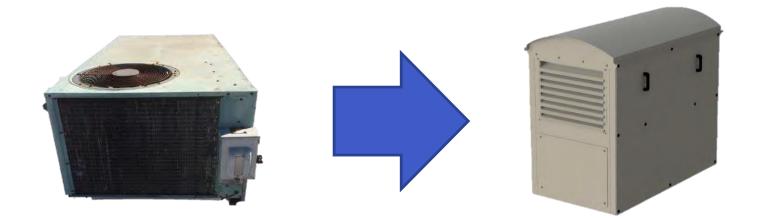




Dedicated Outdoor Air System



- → **PART 1:** Establish Baseline Conditions
- → **PART 2:** Calibrated Baseline Energy Model
- → PART 3: DOAS Conversion
- > PART 4: Establish Post-Conversion Conditions
- → PART 5: Calibrated Post-Conversion Energy Model
- → **PART 6:** Calculate Energy Savings

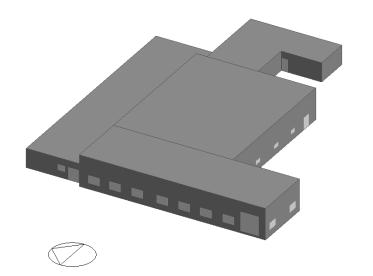


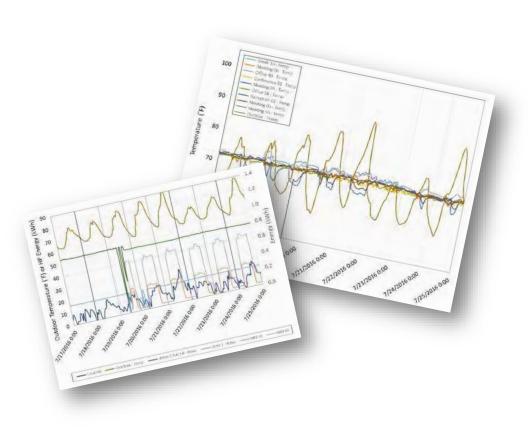
→ **PART 1:** Establish Baseline Conditions

- → Site Review
- → Baseline Air Leakage Testing
- → Installation of Monitoring Equipment



- → PART 2: Calibrated Baseline Energy Model
 - → Actual Operating Conditions (occupancy, schedules, heating and cooling setpoints, etc.)
 - → Baseline Air Tightness
 - → Monitoring Data
 - → Historic Utility Data





→ PART 3: DOAS Conversion

- → New HRV unit
- → Zone-level heating and cooling
- \rightarrow Local design teams and contractors





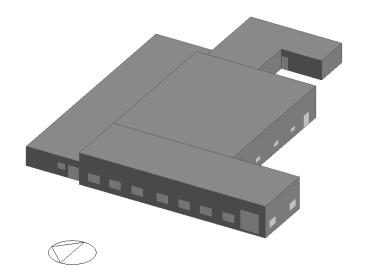
→ PART 4: Establish Post-Conversion Conditions

- → Site Review
- → Post-Conversion Air Leakage Testing
- Additional Monitoring Equipment



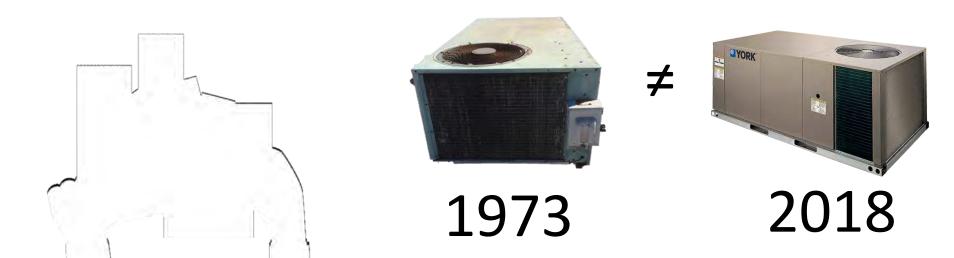
→ PART 5: Calibrated Post-Conversion Energy Model

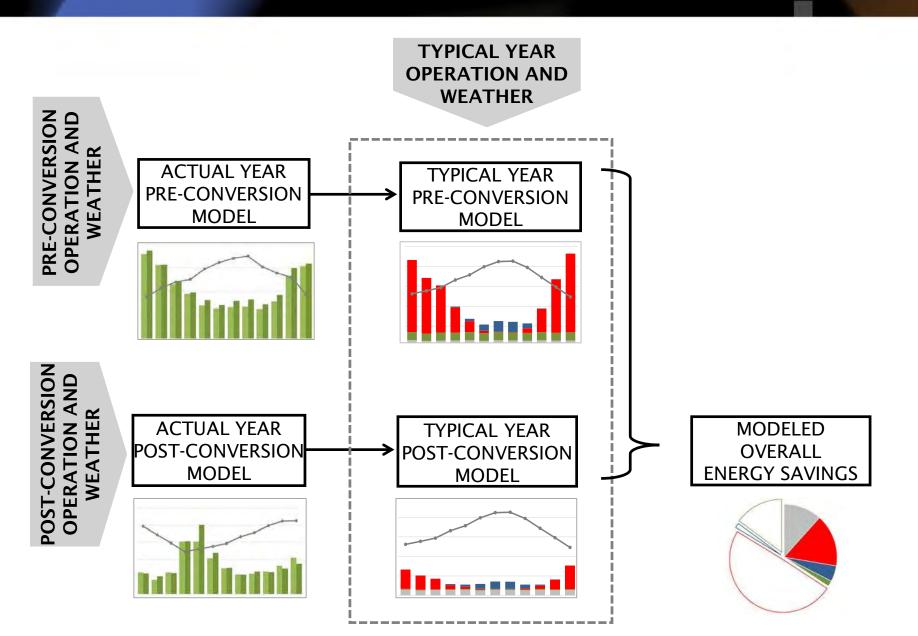
- → Maintain Baseline Operating Conditions
- → Post-Conversion Air Tightness
- → Monitoring Data
- → 1 Year Post Conversion Utility Data

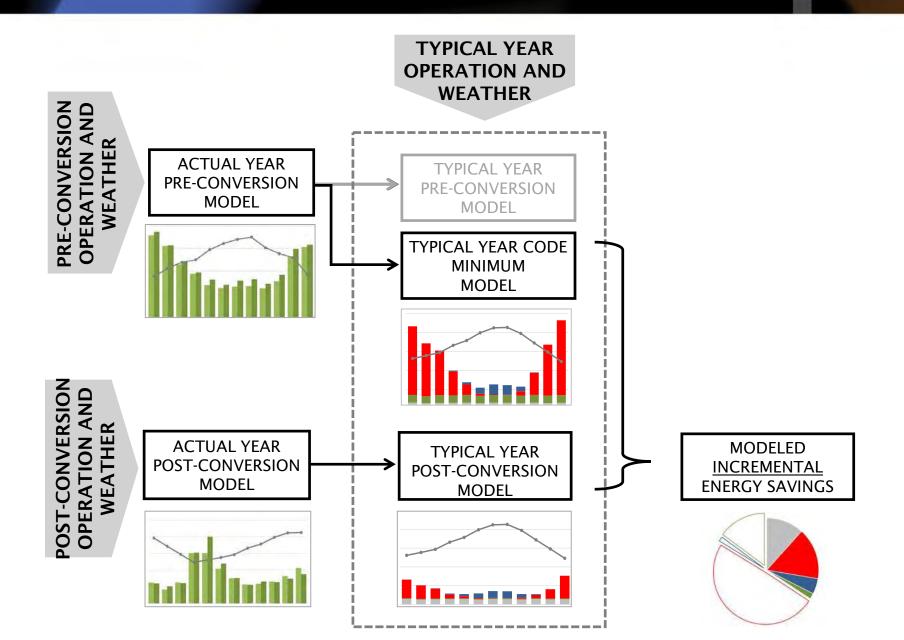




- → PART 6: Calculate Energy Savings
 - → Overall Savings vs. Existing System
 - > i.e. owner utility bills
 - → Incremental Savings vs. New Like-for-Like Replacement
 - > New equipment = higher efficiency, better controls, opportunity to commission, etc.
 - > Aligns with utility incentive programs (& other programs)

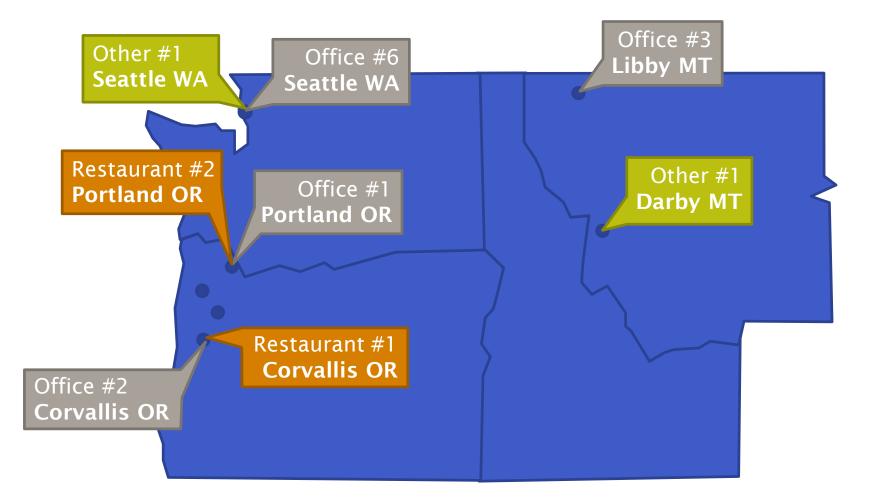








\rightarrow 8 pilot projects



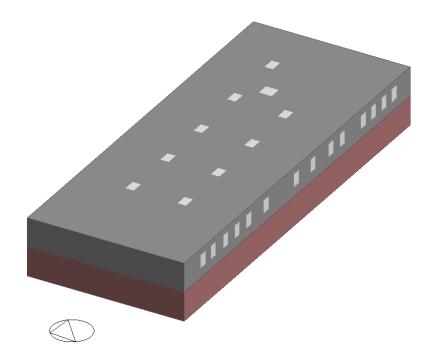




→ Office 1

- \rightarrow Existing heritage building
- → Second floor of a 2 storey building
- \rightarrow Private offices
- → Intermittent occupancy in meeting and conference rooms
- → Monday through Friday day time operation



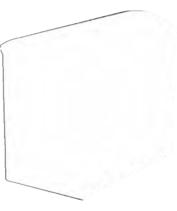




- → Office 1
- \rightarrow Baseline
 - → 9 RTUs, total 35 tons cooling, 650,000 Btu/h heating
- \rightarrow Conversion
 - \rightarrow 4 HRVs
 - → 2 VRF outdoor heat pump units + 8 zone-level VRF fan coil units, 16 tons cooling, 210,000 Btu/h heating













→ Office 1

- → Pre-Conversion Air Leakage Testing
 - \rightarrow Air Leakage Test Result: 0.616 cfm/ft² at 75 Pa
 - Air leakage noted at operable windows, HVAC dampers, and mechanical chases between floors.



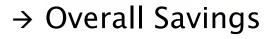
TABLE 1 – SUMMARY OF AIR LEAKAGE TEST RESULTS					
Test Condition	Depressurize	Pressurize	Average		
Enclosure Airtightness [cfm/ft²@75Pa]	0.615	0.617	0.616		
Equivalent Leakage Area [ft² @ 75Pa]	14.9	15.0	14.95		
Air Changes [per Hour @ 50Pa]	5.71	5.84	5.77		
Air Leakage Test Coefficient (C) [cfm/Pa [®]]	1431.3	1761.1	N/A		
Flow Exponent (n) [dimensionless]	0.611	0.564	N/A		
Squared Correlation Coefficient (r²) [dimensionless]	0.9964	0.9977	N/A		



\rightarrow Office 1

- → Post-Conversion Air Leakage Testing
 - → Air Leakage Test Result: 0.506 cfm/ft² at 75 Pa
 - > Improved air leakage between floors

TABLE 1 – SUMMARY OF AIR LEAKAGE TEST RESULTS				
Test Condition	Depressurize	Pressurize	Average	
Enclosure Airtightness [cfm/ft²@75Pa]	0.481	0.531	0.506	
Equivalent Leakage Area [ft² @ 75Pa]	11.87	12.72	12.30	
Air Changes [per Hour @ 50Pa]	4.53	4.96	4.74	
Air Leakage Test Coefficient (C) [cfm/Paª]	1299.4	1306.5	N/A	
Flow Exponent (n) [dimensionless]	0.577	0.598	N/A	
Squared Correlation Coefficient (r²) [dimensionless]	0.9956	0.9980	N/A	



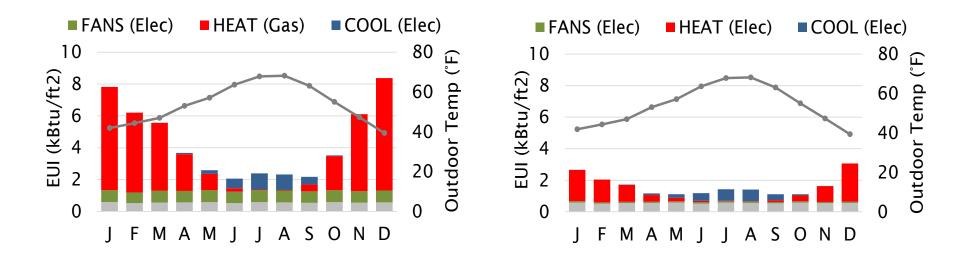
- \rightarrow Existing System: 56 kBtu/ft²
- → DOAS HRV System: 19 kBtu/ft²

37 kBtu/ft²

66% Total Savings

RDH

75% HVAC Savings



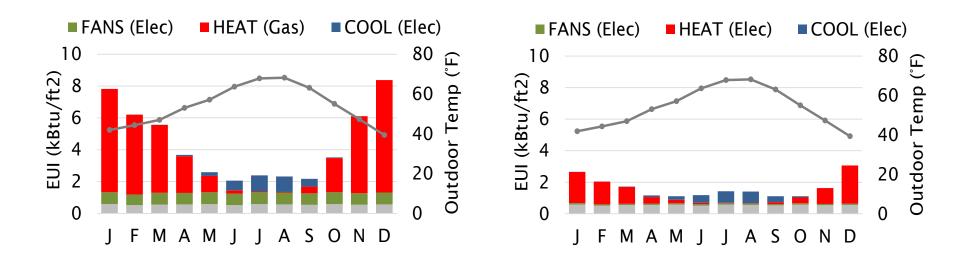
→ Incremental Savings

- \rightarrow New RTU System: 51 kBtu/ft²
- → DOAS HRV System: 19 kBtu/ft²

32 kBtu/ft²

63% Total Savings

72% HVAC Savings







- → Incremental Savings
 - → New gas-fired RTUs vs new electric heat pump RTU
 - → Some utility incentive programs require electric vs electric



Energy Modeling as a Tool to Quantify Savings

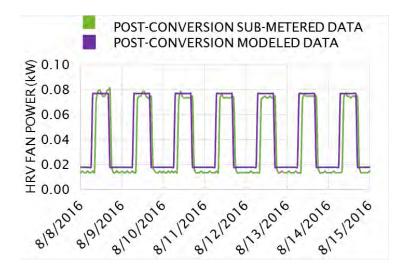
- \rightarrow What we learned:
 - → Normal model calibration things apply

- \rightarrow Low HRV fan power
- → Core bypass & economizer controls
- → VAV DOAS
- → Winter heat pump operation
- → Sidebar: Poor in-service RTU performance

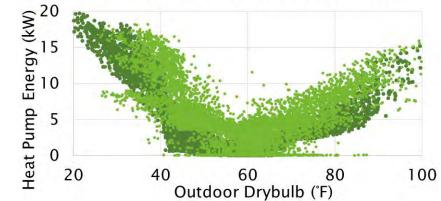
\rightarrow Normal model calibration things apply



\rightarrow Monitoring data



2016/2017 POST-CONVERSION SUB-METERED DATA
2016/2017 POST-CONVERSION MODELED DATA
20



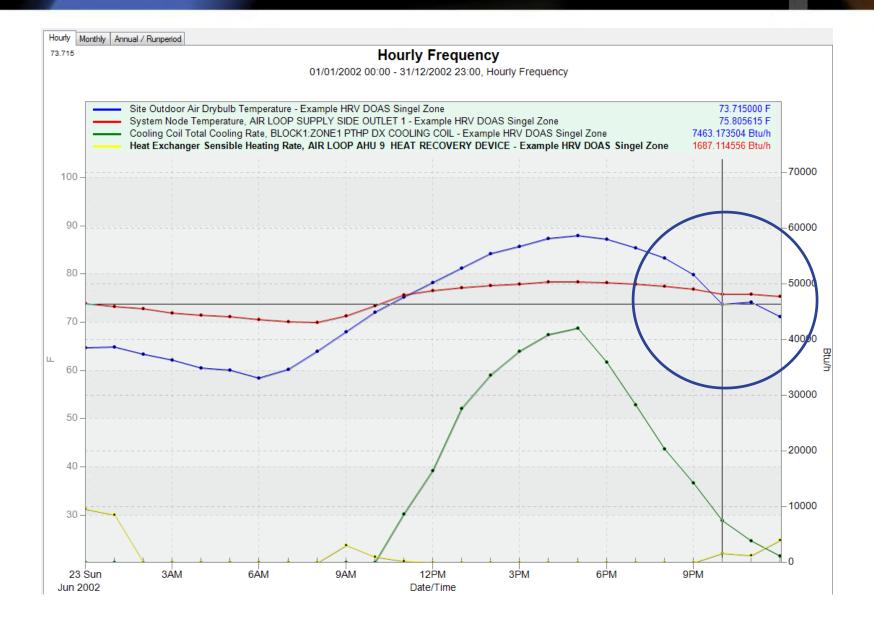
- \rightarrow Low HRV fan power
 - \rightarrow Measured HRV fan power is generally low
 - > 0.2 W/cfm to 0.6 W/cfm
 - → Fan power increases if:
 - Complicated rooftop install
 - Complicated downstream ductwork
 - > Downstream tempering coils (i.e. HRV "post heater")

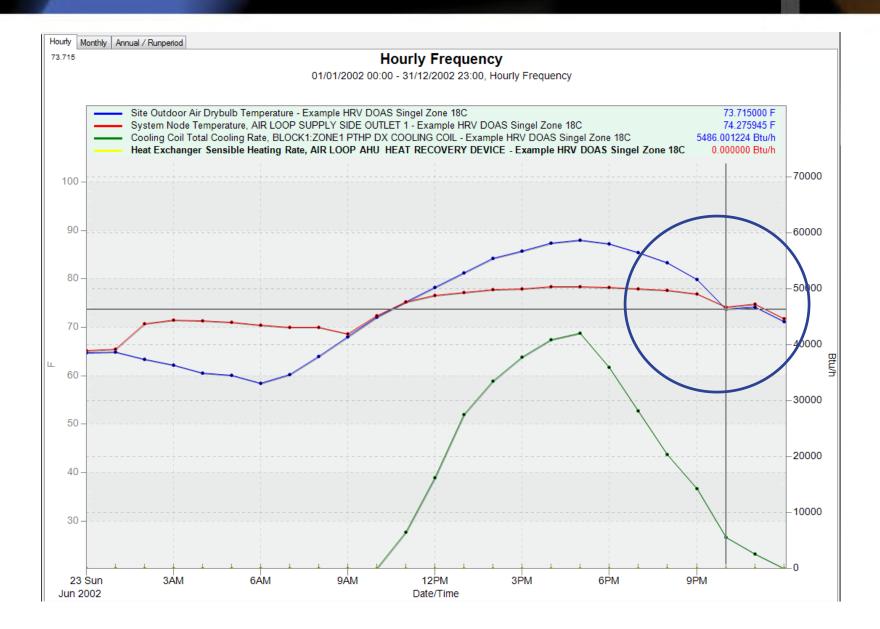
RD -





- → Core bypass & economizer controls
 - → Supply air outlet temperature control
 - > No heat recovery when it is detrimental for cooling
 - → "Boost" mode operation approximated by post-process calculation
 - > Run model at HRV design flow for ventilation (say, 450 cfm)
 - > Run model at HRV "boost" flow for cooling (say, 1000 cfm)
 - > Compare hourlies and swap cooling and fan power

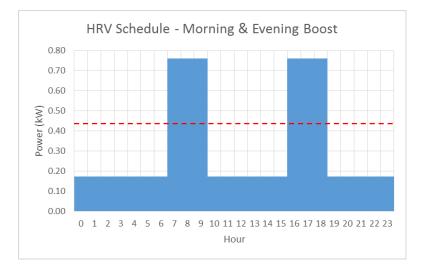






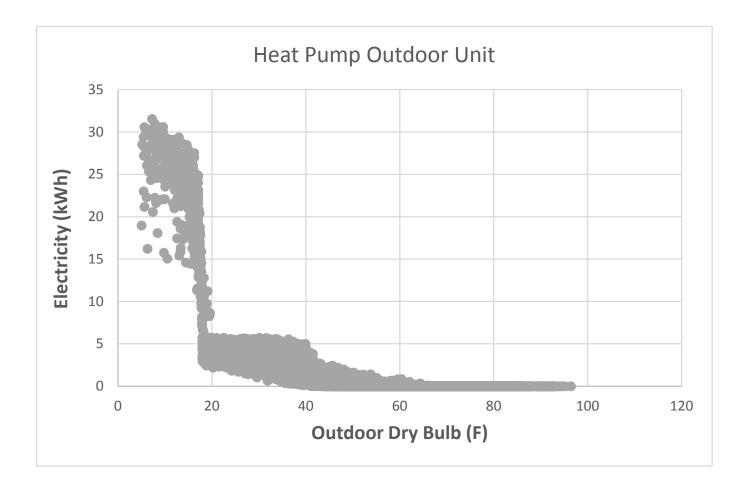
\rightarrow VAV DOAS

- → Approximating VAV as "average" CV
- → Consider impact on peak load

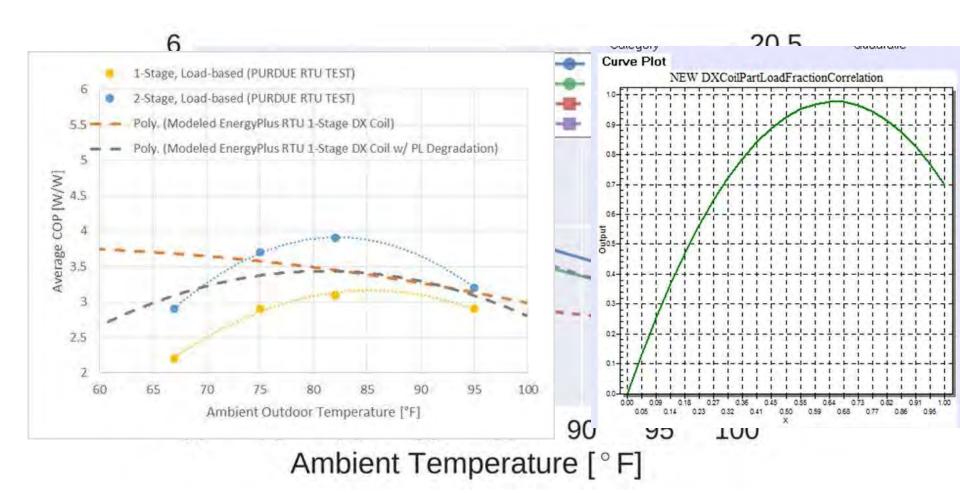


Hour	kW	cfm
0	0.17	589
1	0.17	589
2	0.17	589
3	0.17	589
4	0.17	589
5	0.17	589
6	0.17	589
7	0.76	970
8	0.76	970
9	0.76	970
10	0.17	589
11	0.17	589
12	0.17	589
13	0.17	589
14	0.17	589
15	0.17	589
16	0.76	970
17		970
18	0.76	970
19	0.17	589
20	0.17	589
21	0.17	589
22	0.17	589
23	0.17	589
	AVG	684

\rightarrow Winter heat pump operation



→ Sidebar: Poor in-service RTU performance





Questions

 \rightarrow neea.org

→ betterbricks.com





Discussion + Questions

FOR FURTHER INFORMATION PLEASE VISIT

→ rdh.com | buildingsciencelabs.com

RD – BUILDING SCIENCE

RDH Building Engineering Ltd. and Building Science Consulting Inc. have merged. Effective November 1, 2015, we now operate as one integrated firm. The merger brings two of the leading building science firms in North America together to provide a combination of cutting-edge research with leading design and implementation capabilities. The result is a unique offering for our clients-an ability to explore new and innovative ideas based on science and our practical knowledge of what can be built. We are excited about the possibilities as we launch the new firm.